reader a familiarity with the device and the ability to perform MOSFET circuit analysis both rapidly and effectively.

In the following examples, to keep matters simple and thus focus attention on the essence of MOSFET circuit operation, we will generally neglect channel-length modulation; that is, we will assume $\lambda = 0$. We will find it convenient to work in terms of the overdrive voltage; $V_{ov} = V_{GS} - V_{tn}$ for NMOS and $|V_{ov}| = V_{SG} - |V_{tp}|$ for PMOS.

### Example 5.3

Design the circuit of Fig. 5.21: that is, determine the values of $R_D$ and $R_S$ so that the transistor operates at $I_D = 0.4$ mA and $V_D = +0.5$ V. The NMOS transistor has $V_t = 0.7$ V, $\mu_nC_{ox} = 100$ $\mu$A/V$^2$, $L = 1$ $\mu$m, and $W = 32$ $\mu$m. Neglect the channel-length modulation effect (i.e., assume that $\lambda = 0$).

![Figure 5.21 Circuit for Example 5.3.](image)

#### Solution

To establish a dc voltage of $+0.5$ V at the drain, we must select $R_D$ as follows:

$$R_D = \frac{V_{DD} - V_D}{I_D} = \frac{2.5 - 0.5}{0.4} = 5 \text{ k}\Omega$$

To determine the value required for $R_S$, we need to know the voltage at the source, which can be easily found if we know $V_{GS}$. This in turn can be determined from $V_{ov}$. Toward that end, we note that since $V_D = 0.5$ V is greater than $V_t$, the NMOS transistor is operating in the saturation region, and we can use the saturation-region expression of $i_D$ to determine the required value of $V_{ov}$,

$$I_D = \frac{1}{2} \mu_nC_{ox} \frac{W}{L} V_{ov}^2$$

Then substituting $I_D = 0.4$ mA = $400$ $\mu$A, $\mu_nC_{ox} = 100$ $\mu$A/V$^2$, and $W/L = 32/1$ gives

$$400 = \frac{1}{2} \times 100 \times \frac{32}{1} V_{ov}^2$$

\[ \text{Solve for } V_{ov}: \]
Example 5.3 continued

which results in

\[ V_{OV} = 0.5 \text{ V} \]

Thus,

\[ V_{GS} = V_t + V_{OV} = 0.7 + 0.5 = 1.2 \text{ V} \]

Referring to Fig. 5.21, we note that the gate is at ground potential. Thus, the source must be at –1.2 V, and the required value of \( R_s \) can be determined from

\[
R_s = \frac{V_s - V_{SS}}{I_D}
= \frac{-1.2 - (-2.5)}{0.4}
= 3.25 \text{ k}\Omega
\]

EXERCISE

D5.8 Redesign the circuit of Fig. 5.21 for the following case: \( V_{DD} = -V_{SS} = 2.5 \text{ V}, \ V_t = 1 \text{ V}, \ \mu_nC_{ox} = 60 \mu \text{A/V}^2, W/L = 120 \mu \text{m}/3 \mu \text{m}, \ I_D = 0.3 \text{ mA}, \text{ and } V_D = +0.4 \text{ V}. \)

Ans. \( R_D = 7 \text{ k}\Omega; \ R_s = 3.3 \text{ k}\Omega \)

Example 5.4

Figure 5.22 shows an NMOS transistor with its drain and gate terminals connected together. Find the \( i-v \) relationship of the resulting two-terminal device in terms of the MOSFET parameters \( k_n = k'_n(W/L) \) and \( V_{tn} \). Neglect channel-length modulation (i.e., \( \lambda = 0 \)). Note that this two-terminal device is known as a diode-connected transistor.

[Figure 5.22]
Solution

Since \( v_D = v_G \) implies operation in the saturation mode,

\[
i_D = \frac{1}{2} k_n' \left( \frac{W}{L} \right) (v_{GS} - V_{tn})^2
\]

Now, \( i = i_D \) and \( v = v_{GS} \), thus

\[
i = \frac{1}{2} k_n \left( \frac{W}{L} \right) (v - V_{tn})^2
\]

Replacing \( k_n \left( \frac{W}{L} \right) \) by \( k_n \) results in

\[
i = \frac{1}{2} k_n (v - V_{tn})^2
\]

EXERCISES

D5.9 For the circuit in Fig. E5.9, find the value of \( R \) that results in \( V_D = 0.7 \) V. The MOSFET has \( V_m = 0.5 \) V, \( \mu_n C_{ox} = 0.4 \) mA/V\(^2\), \( W/L = \frac{0.72 \mu m}{0.18 \mu m} \), and \( \lambda = 0 \).

Ans. 34.4 k\( \Omega \)

\[\begin{align*}
&+1.8 \text{ V} \\
&\downarrow \\
&R \\
&\downarrow \\
&V_D \\
&\downarrow \\
&\downarrow \\
&\downarrow \\
&Q_1
\end{align*}\]

Figure E5.9

D5.10 Figure E5.10 shows a circuit obtained by augmenting the circuit of Fig. E5.9 considered in Exercise 5.9 with a transistor \( Q_2 \) identical to \( Q_1 \) and a resistance \( R_2 \). Find the value of \( R_2 \) that results in \( Q_2 \) operating at the edge of the saturation region. Use your solution to Exercise 5.9.

Ans. 50 k\( \Omega \)
Example 5.5

Design the circuit in Fig. 5.23 to establish a drain voltage of 0.1 V. What is the effective resistance between drain and source at this operating point? Let $V_{tn} = 1$ V and $k'(W/L) = 1 \text{mA/V}^2$.

Solution

Since the drain voltage is lower than the gate voltage by 4.9 V and $V_{gs} = 1$ V, the MOSFET is operating in the triode region. Thus the current $I_D$ is given by

$$I_D = k' \frac{W}{L} \left[ (V_{gs} - V_{tn})V_{ds} - \frac{1}{2} V_{ds}^2 \right]$$

$$I_D = 1 \times \left[ (5 - 1) \times 0.1 - \frac{1}{2} \times 0.01 \right]$$

$$= 0.395 \text{mA}$$
The required value for \( R_D \) can be found as follows:

\[
R_D = \frac{V_{DD} - V_D}{I_D}
\]

\[
= \frac{5 - 0.1}{0.395} = 12.4 \text{ k}\Omega
\]

In a practical discrete-circuit design problem, one selects the closest standard value available for, say, 5% resistors—in this case, 12 k\( \Omega \); see Appendix J. Since the transistor is operating in the triode region with a small \( V_{DS} \), the effective drain-to-source resistance can be determined as follows:

\[
r_{DS} = \frac{V_{DS}}{I_D}
\]

\[
= \frac{0.1}{0.395} = 253 \text{ \Omega}
\]

Alternatively, we can determine \( r_{DS} \) by using the formula

\[
r_{DS} = \frac{1}{k_n V_{OV}}
\]

to obtain

\[
r_{DS} = \frac{1}{1 \times (5 - 1)} = 0.25 \text{ k}\Omega = 250 \text{ \Omega}
\]

which is close to the value found above.

**EXERCISE**

5.11 If in the circuit of Example 5.5 the value of \( R_D \) is doubled, find approximate values for \( I_D \) and \( V_D \).

**Ans.** 0.2 mA; 0.05 V

**Example 5.6**

Analyze the circuit shown in Fig. 5.24(a) to determine the voltages at all nodes and the currents through all branches. Let \( V_m = 1 \text{ V} \) and \( k_n(W/L) = 1 \text{ mA/V}^2 \). Neglect the channel-length modulation effect (i.e., assume \( \lambda = 0 \)).
Example 5.6 continued

\( R_{G1} = 10 \, \text{M}\Omega \)
\( R_G = 6 \, \text{k}\Omega \)
\( R_{G2} = 10 \, \text{M}\Omega \)
\( R_D = 6 \, \text{k}\Omega \)
\( V_{DD} = +10 \, \text{V} \)
\( +10 \, \text{V} \)
\( 0.5 \, \mu\text{A} \)
\( 10 \, \text{M}\Omega \)
\( 10 \, \text{M}\Omega \)
\( 10 \, \text{M}\Omega \)
\( 10 \, \text{M}\Omega \)
\( 6 \, \text{k}\Omega \)
\( 6 \, \text{k}\Omega \)
\( 6 \, \text{k}\Omega \)
\( 6 \, \text{k}\Omega \)
\( V_{GS} = +5 \, \text{V} \)
\( 10 \, \text{M}\Omega \)
\( 0 \)
\( 10 - 6 \, I_D \)
\( 6 \, \text{M}\Omega \)
\( 6 \, \text{M}\Omega \)
\( 6 \, \text{M}\Omega \)
\( 6 \, \text{M}\Omega \)
\( I_D \)
\( I_D \)

**Figure 5.24** (a) Circuit for Example 5.6. (b) The circuit with some of the analysis details shown.

**Solution**

Since the gate current is zero, the voltage at the gate is simply determined by the voltage divider formed by the two 10-M\(\Omega\) resistors,

\[
V_G = V_{DD} \frac{R_{G2}}{R_{G2} + R_{G1}} = 10 \times \frac{10}{10 + 10} = +5 \, \text{V}
\]

With this positive voltage at the gate, the NMOS transistor will be turned on. We do not know, however, whether the transistor will be operating in the saturation region or in the triode region. We shall assume saturation-region operation, solve the problem, and then check the validity of our assumption. Obviously, if our assumption turns out not to be valid, we will have to solve the problem again for triode-region operation.

Refer to Fig. 5.24(b). Since the voltage at the gate is 5 V and the voltage at the source is \( I_D \) (mA) \( \times \) 6 (k\(\Omega\)) = 6\( I_D \) (V), we have

\[
V_{GS} = 5 - 6I_D
\]

Thus \( I_D \) is given by

\[
I_D = \frac{1}{2} k_n W \frac{V_{GS} - V_n}{L}^2
\]

\[
= \frac{1}{2} \times 1 \times (5 - 6I_D - 1)^2
\]
which results in the following quadratic equation in $I_D$:

$$18I_D^2 - 25I_D + 8 = 0$$

This equation yields two values for $I_D$: 0.89 mA and 0.5 mA. The first value results in a source voltage of $6 \times 0.89 = 5.34$ V, which is greater than the gate voltage and does not make physical sense as it would imply that the NMOS transistor is cut off. Thus,

$$I_D = 0.5 \text{ mA}$$

$$V_S = 0.5 \times 6 = +3 \text{ V}$$

$$V_{GS} = 5 - 3 = 2 \text{ V}$$

$$V_D = 10 - 6 \times 0.5 = +7 \text{ V}$$

Since $V_D > V_G - V_{tn}$, the transistor is operating in saturation, as initially assumed.

**EXERCISES**

5.12 For the circuit of Fig. 5.24, what is the largest value that $R_D$ can have while the transistor remains in the saturation mode?

**Ans.** 12 kΩ

D5.13 Redesign the circuit of Fig. 5.24 for the following requirements: $V_{DD} = +5 \text{ V}$, $I_D = 0.32$ mA, $V_S = 1.6 \text{ V}$, $V_D = 3.4 \text{ V}$, with a 1-μA current through the voltage divider $R_{g1}, R_{g2}$. Assume the same MOSFET as in Example 5.6.

**Ans.** $R_{g1} = 1.6 \text{ MΩ}$; $R_{g2} = 3.4 \text{ MΩ}$, $R_S = R_D = 5 \text{ kΩ}$

**Example 5.7**

Design the circuit of Fig. 5.25 so that the transistor operates in saturation with $I_D = 0.5 \text{ mA}$ and $V_D = +3 \text{ V}$. Let the PMOS transistor have $V_{tp} = -1 \text{ V}$ and $k_p(W/L) = 1 \text{ mA/V}^2$. Assume $\lambda = 0$. What is the largest value that $R_D$ can have while maintaining saturation-region operation?
Example 5.7 continued

\[ I_D = \frac{1}{2} |V_{GW}| W \frac{K_p}{L} |V_{GW}|^2 \]

Substituting \( I_D = 0.5 \text{ mA} \) and \( \frac{K_p W}{L} = 1 \text{ mA/V}^2 \), we obtain

\[ |V_{GW}| = 1 \text{ V} \]

and

\[ V_{SG} = \frac{V_p}{2} + |V_{GW}| = 1 + 1 = 2 \text{ V} \]

Since the source is at +5 V, the gate voltage must be set to +3 V. This can be achieved by the appropriate selection of the values of \( R_{G1} \) and \( R_{G2} \). A possible selection is \( R_{G1} = 2 \Omega \) and \( R_{G2} = 3 \Omega \).

The value of \( R_D \) can be found from

\[ R_D = \frac{V_D}{I_D} = \frac{3}{0.5} = 6 \text{ k}\Omega \]

Saturation-mode operation will be maintained up to the point that \( V_D \) exceeds \( V_C \) by \( |V_p| \); that is, until

\[ V_{D_{\text{max}}} = 3 + 1 = 4 \text{ V} \]

This value of drain voltage is obtained with \( R_D \) given by

\[ R_D = \frac{4}{0.5} = 8 \text{ k}\Omega \]
**EXERCISE**

**D5.14** For the circuit in Fig. E5.14, find the value of $R$ that results in the PMOS transistor operating with an overdrive voltage $|V_{OV}| = 0.6 \, \text{V}$. The threshold voltage is $V_{tp} = -0.4 \, \text{V}$, the process transconductance parameter $k'_p = 0.1 \, \text{mA/V}^2$, and $W/L = 10 \, \mu\text{m}/0.18 \, \mu\text{m}$.

**Ans.** $800 \, \Omega$

![Figure E5.14](image-url)

**Example 5.8**

The NMOS and PMOS transistors in the circuit of Fig. 5.26(a) are matched, with $k'_n(W_n/L_n) = k'_p(W_p/L_p) = 1 \, \text{mA/V}^2$ and $V_{tn} = -V_{tp} = 1 \, \text{V}$. Assuming $\lambda = 0$ for both devices, find the drain currents $i_{DN}$ and $i_{DP}$, as well as the voltage $v_{O}$, for $v_I = 0 \, \text{V}$, $+2.5 \, \text{V}$, and $-2.5 \, \text{V}$.

![Figure 5.26](image-url)

**Figure 5.26** Circuits for Example 5.8.
Example 5.8 continued

Solution

Figure 5.26(b) shows the circuit for the case \( v_I = 0 \) V. We note that since \( Q_N \) and \( Q_P \) are perfectly matched and are operating at equal values of \(|V_{GS}| = 2.5\) V, the circuit is symmetrical, which dictates that \( v_O = 0 \) V. Thus both \( Q_N \) and \( Q_P \) are operating with \(|V_{DS}| = 0\) and, hence, in saturation. The drain currents can now be found from

\[
I_{DP} = I_{DN} = \frac{1}{2} \times 1 \times (2.5 - 1)^2 = 1.125 \text{ mA}
\]

Next, we consider the circuit with \( v_I = +2.5 \) V. Transistor \( Q_P \) will have a \( V_{GS} \) of zero and thus will be cut off, reducing the circuit to that shown in Fig. 5.26(c). We note that \( v_O \) will be negative, and thus \( v_{GD} \) will be greater than \( V_{th} \), causing \( Q_N \) to operate in the triode region. For simplicity we shall assume that \( v_{DS} \) is small and thus use

\[
I_{DN} \approx k' (W_n/L_n) (V_{GS} - V_m) V_{DS} \\
= 1 [2.5 - (-2.5) - 1][v_O - (-2.5)]
\]

From the circuit diagram shown in Fig. 5.26(c), we can also write

\[
I_{DN} (\text{mA}) = \frac{0 - v_O}{10 (k\Omega)}
\]
These two equations can be solved simultaneously to yield

\[ I_{DN} = 0.244 \text{ mA} \quad v_O = -2.44 \text{ V} \]

Note that \( V_{DS} = -2.44 - (-2.5) = 0.06 \text{ V}, \) which is small as assumed.

Finally, the situation for the case \( v_I = -2.5 \text{ V} [\text{Fig. 5.26(d)}] \) will be the exact complement of the case \( v_I = +2.5 \text{ V} \): Transistor \( Q_N \) will be off. Thus \( I_{DN} = 0, \) \( Q_P \) will be operating in the triode region with \( I_{DP} = 0.244 \text{ mA} \) and \( v_O = +2.44 \text{ V}. \)

**EXERCISE**

5.15 The NMOS and PMOS transistors in the circuit of Fig. E5.15 are matched with \( k'_n (W_n/L_n) = k'_p (W_p/L_p) = 1 \text{ mA/V}^2 \) and \( V_n = -V_p = 1 \text{ V}. \) Assuming \( \lambda = 0 \) for both devices, find the drain currents \( i_{DN} \) and \( i_{DP} \) and the voltage \( v_O \) for \( v_I = 0 \text{ V}, +2.5 \text{ V}, \) and \( -2.5 \text{ V}. \)

**Ans.** \( v_I = 0 \text{ V}: \) 0 mA, 0 mA, 0 V; \( v_I = +2.5 \text{ V}: \) 0.104 mA, 0 mA, 1.04 V; \( v_I = -2.5 \text{ V}: \) 0 mA, 0.104 mA, -1.04 V

![Figure E5.15](image)

**Concluding Remark** If a MOSFET is conducting but its mode of operation (saturation or triode) is not known, we assume operation in the saturation region, solve the problem, and check whether the conditions for saturation-mode operation are satisfied. If not, then the MOSFET is operating in the triode region and the analysis is done accordingly.